Effect of slip on Herschel- Bulkley Fluid Flow Through An Artery With Stenosis and Post Stenotic Dilatation

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Abstract: Slip effect on steady Herschel-Bulkley fluid flow through a tube with stenosis and post stenosis dilation have been investigated. It is assumed that the stenosis is mild. The analytical expressions are obtained for resistance to the flow, velocity, and pressure drop and wall shear stress. The different parameters effects on the flow rate, shear stress and stream lines are discussed and presented graphically.

Keywords : Herschel-Bulkley fluid, Slip velocity, Stenoses, Dilatation.

1. INTRODUCTION

Cardiovascular diseases are one of the major health problems one such is atherosclerosis. The malfunction of blood flow due to stenosis causes a severe circulatory disorder. The entire cardiovascular system is affected due to the presence of stenosis and because of this it is one of the interesting areas of research.

Shukla et. al.[15] studied the non-Newtonian behaviour of blood flow in the stenosed artery, whereas Mishra et al. [8] analysed by considering stenosed artery of a uniform cross-section. Sreenadh et al. [17] developed a mathematical model to study the multiple stenosis influence. Many researcher have developed various type of Mathematical models to study the flow of Blood through channel with variable cross-section (Shukla [14]), by treating blood as a Newtonian fluid. It is seen that blood behaves Herschel-Bulkley fluid in small diameter tube (Chaturani *et.al.*[4]). Many researchers have studied the blood flow through stenosed arteries by treating as Herschel-Bulkley fluid (Biswas and Laskar [3]).

Tandon, *et. al.* [18] described a mathematical model to understand the post-stenotic dilatation problem by treating blood as Casson fluid . A K Singh *et.al* [16] have studied the resistance to the flow ratio for yield stress by considering blood flow in small artery having stenosis and post stenotic dilatation. Sanjeev *et. al.* [13] represented blood flow resistance for a small artery with multiple stenoses & post-stenotic dilatation and Maruthi Prasad *et. al.* [6] examined post-stenotic dilatation by considering the blood as a Jeffrey fluid. Pincombe *et. al.* [11] have studied influence of multiple stenosis and post stenotic dilatation in small arteries by considering blood as non-Newtonian.

Arun Kumar [1] analysed the influence of multiple stenoses and post-dilatation on blood flow through an artery by considering fluid as Herschel-Bulkley. Multiple stenotic effects on blood flow in the presence of slip was investigated by Arun Kumar [2]. The flow of blood through uniform and stenosed tubes under the effect of slip velocity are studied by Philip and Chandra [10]. The effect of slip condition on fluid flow through the porous medium with stenosis by considering fluid as couple stress studied by G Radhakrishnamacharya *et. al.* [5]. By taking narrow tubes G. Radhakrishnamacharya *et. al.* [9] examined the slip effect on H-B fluid.

Priyadarshini *et. al.* [12] have analyzed the flow of Herschel-Bulkley fluid through a tapered arterial stenosis with dilatation. K M Prasad *et. al.* [7] investigated the effect of stenosis and post-stenotic dilatation by treating blood as Herschel-Bulkley fluid. Motivated by these studies an attempt is made in this paper to study the slip effect on Stenosis and poststenotic dilatation by considering blood as Herschel-Bulkley.

2. MATHEMATICAL FORMULATION

In the present study we considered the steady flow of H-B fluid through a circular artery containing multiple abnormal segments.



Figure. 1:Geometry of the problem

The geometry of the wall of the tube is taken as ([K Maruti Prasad *et.al* [7])

$$h = \frac{R(z)}{R_o} \begin{cases} 1 - \frac{\delta_i}{2R_o} \left[1 + \cos \frac{2\pi}{L_i} \left(z - \alpha_i - \frac{L_i}{2} \right) \right], \\ \alpha_i \le z \le \beta_i \end{cases}$$

$$(1, otherwise)$$

The radius of the artery at dilatation, normal artery and length of the i^{th} abnormal segement is represented by R, R_o , L_i respectively. The max. distance of the i^{th} abnormal segment is given by δ_i and it is +ve, -ve for stenosis and aneurysms respectively. The distance from the origin to the beginning of the i^{th} abnormal segment is denoted by α_i and it is given as

$$\alpha_{i} = \left[\sum_{j=1}^{i} \left(d_{j} + L_{j}\right)\right] - L_{i}$$
(2)

The distance from the origin to the end of the

 i^{th} abnormal segment is given by eta_i , i.e

$$\beta_{i} = \left[\sum_{j=1}^{i} \left(d_{j} + l_{j}\right)\right] \tag{3}$$

Where d_i is the distance of i^{th} and $(i-1)^{th}$ start and end abnormal segment respectively given by [14].

By considering the circular cross-section on an artery under mild stenosis condition the general equation is given as

$$\frac{1}{r}\frac{\partial}{\partial r}(r\tau) = -\frac{\partial p}{\partial r} \tag{4}$$

Where τ is the shear stress for H-B fluid and given by

$$\tau = \left(-\frac{\partial w}{\partial r}\right)^n + \tau_o \text{ if } \tau \ge \tau_o \tag{5}$$

$$\frac{\partial w}{\partial r} = 0 \quad \text{if} \quad \tau < \tau_o \tag{6}$$

Where (r, z) are cylindrical polar co-ordinates with

z is along the tube where as r is along the normal to the axis of the tube. P is pressure, τ is shear stress and τ_o is yield and w is the velocity of the fluid and n is the power law index.

The boundary conditions are:

(i)
$$\tau \Big|_{r=0}$$
 is finite at (7)

(ii)
$$\left. \frac{\partial w}{\partial r} \right|_{r=h(z)} = \frac{-\alpha}{Ro\sqrt{Da}} w$$
 (8)

Where the slip parameter is represented by α , permeability parameter Da and radius of the tube is Ro.

3. SOLUTION

(1)

The velocity is calculated by solving equations. (5-6), by using the boundary conditions (7-8) we obtained,

$$w = \frac{h^{m+1}P^m}{2^m (m+1)} \begin{bmatrix} \left(1 - \frac{2\tau_o}{hP}\right)^{m+1} - \left(\frac{r}{h} - \frac{2\tau_o}{hP}\right)^{m+1} \\ + \frac{R_o \sqrt{Da}}{\alpha} \frac{(m+1)}{h} \left(1 - \frac{2\tau_o}{hP}\right)^m \end{bmatrix}$$
(9)

Where $P = -\frac{\partial p}{\partial z}$ and $w = \frac{1}{n}$

The plug flow region is obtained by applying boundary condition (6) 2^{-1}

$$r_o = \frac{2\tau_o}{P} \tag{10}$$

By applying the condition $\tau = \tau_h$ at r = h we get

$$\frac{r_o}{h} = \frac{\tau_o}{\tau_h} = \tau , \quad 0 < \tau < 1 \tag{11}$$

Taking $r = r_o$ in equation (9), the plug core velocity is

$$w_{p} = \frac{h^{m+1}P^{m}}{2^{m}(m+1)} \left[\left(1 - \frac{r_{o}}{h} \right)^{m+1} + \frac{R_{o}\sqrt{Da}}{\alpha} \frac{(m+1)}{h} \left(1 - \frac{r_{o}}{h} \right)^{m} \right]$$
for $0 \le r \le r_{o}$ (12)

Q is volumetric flow rate defined as

$$Q = 2 \left[\int_{0}^{r_o} w_p \ r \, dr + \int_{r_o}^{r_h} w \ r \, dr \right]$$
(13)

On integrating we get

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$$Q = \frac{P^{m}h^{m+3}\left(1 - \frac{r_{o}}{h}\right)^{m+1}}{2^{m}m_{1}} \times \begin{bmatrix} m_{2} - 2(m+3)\left(1 - \frac{r_{o}}{h}\right) \\ + 2\left(1 - \frac{r_{o}}{h}\right)^{2} + m_{1} \\ \times \frac{R_{o}\sqrt{Da}}{\alpha h^{3}}\left(1 - \frac{r_{o}}{h}\right)^{-1}\left\{r_{o}^{2} + h\left(1 - \frac{r_{o}^{2}}{h^{2}}\right)\right\} \end{bmatrix}$$
(14)

From equation (14)

$$\frac{dp}{dz} = -P = \frac{\left[2^m m_1 Q\right]^{\frac{1}{m}}}{h^{1+\frac{3}{m}} \left(1-\tau\right)^{1+\frac{1}{m}} \left[m_2 - 2m_3 + m_1 \frac{m_4}{\left(1-\tau\right)}\right]}$$
(15)

Where

$$m_{1} = (m+1)(m+2)(m+3)$$

$$m_{2} = (m+2)(m+3)$$

$$m_{3} = (m+3)(1-\tau) + 2(1-\tau)^{2}$$

$$m_{4} = \frac{R_{o}\sqrt{Da}}{\alpha h^{3}} \left\{ \frac{\tau^{2}}{h^{2}} + \frac{1}{h^{2}}(1-\tau^{2}) \right\}$$

The formula for calculating pressure drop Δp is

$$\Delta p = \int_{0}^{l} \frac{dp}{dz} dz$$
(16)
$$\Delta p = \int_{0}^{l} \frac{\left[2^{m} m_{1} Q\right]^{\frac{1}{m}}}{h^{1+\frac{3}{m}} \left[m_{2} \left(1-\tau\right)^{m+1} - 2\left(m+2+\tau\right)\left(1-\tau\right)^{m+2}\right]^{\frac{1}{m}}} dz$$
(17)

Using the following non-dimensional quantities

$$z^* = \frac{z}{L}, \ \delta^* = \frac{\delta}{R_o}, \ R^* = \frac{R(z)}{R_o}, \ P^* = \frac{P}{\left(\mu W L / R_o\right)},$$
$$\tau_o^* = \frac{\tau_o}{\left(\mu W / R_o\right)}, \ \tau^* = \frac{\tau}{\mu \left(W / R_o\right)}, \ Q^* = \frac{Q}{\pi R_o^2 W}$$

In Eqn.(17), we finally get (after dropping asterick)

$$\Delta p = \int_{0}^{l} \frac{\left[2^{m} m_{1} Q\right]^{\frac{1}{m}}}{h^{1+\frac{3}{m}} \left[m_{2} \left(1-\tau\right)^{m+1} - 2\left(m+2+\tau\right)\left(1-\tau\right)^{m+2}\right]^{\frac{1}{m}}} dz$$

$$(18)$$

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 λ is the flow to the resistance given by

$$\lambda = \frac{\Delta p}{Q} = \frac{1}{Q} \int_{0}^{l} \frac{\left[2^{m} m_{1} Q\right]^{\frac{1}{m}}}{h^{1+\frac{3}{m}}} \begin{bmatrix} m_{2} (1-\tau)^{m+1} - 2(m+2+\tau)(1-\tau)^{m+2} \\ + m_{1} m_{4} (1-\tau)^{m} \end{bmatrix}^{\frac{1}{m}} dz$$
(19)

With out stenosis (h = 1) the pressure drop Δp_{\perp} is calculated from Eq. (18) as

$$\Delta p_{N} = \int_{0}^{l} \frac{\left[2^{m} m_{1} Q\right]^{\frac{1}{m}}}{\left[m_{2} \left(1-\tau\right)^{m+1} - 2\left(m+2+\tau\right)\left(1-\tau\right)^{m+2}\right]^{\frac{1}{m}}} dz + m_{1} \frac{R_{o} \sqrt{Da} \left(1-\tau\right)^{m}}{\alpha} \right]^{\frac{1}{m}} dz$$
(20)

The resistance to the flow in the absence of stenosis λ_{N} is obtained from Eq.(20) as,

$$\lambda_{N} = \frac{\Delta p_{N}}{Q} \tag{21}$$

 λ is the normalized resistance to the flow and it is given by

$$\bar{\lambda} = rac{\lambda}{\lambda_N}$$

The wall shear stress is given by

$$\tau_h = -\frac{h}{2} \frac{dp}{dz} \tag{23}.$$

4. RESULT AND DISCUSSISON

The equations for velocity (W), core velocity (W_n) , volumetric flow rate (Q), resistance to the flow

 (λ) , pressure drop (Δp) and wall shear stress (τ_{h}) are given and have been evaluated for various values of corresponding parameters and presented graphically.

It is illustrated from fig. 2 that as permeability parameter (Da) increases flow resistance decreases. Further increases in slip parameter (α) and pow law index increases flow resistance is also increases [figs. (3,4)].

The wall shear stress(τ_h) decreases as permeability decreases and increases with slip parameter (Da) parameter (α) [figs. (5,6)]. It is also observed that pressure drop decreases as permeability parameter (Da) increases, [fig (7)]. Figure 8 and figure 9 demonstrated the steam line in the stenotic regions. It is observed that stenosis increases the resistance

(22)





5. CONCLUSIONS

The steady flow of Herschel Bulkley fluid flow artery with both stenosis through an and dilatations under the influence of slip have been presented. The results have been evaluated and observed that the resistance to the flow decreases with increase with the permeability parameter (Da), power law index, and increases with slip parameter (α) . As wall shear stress decreases as the permeability parameter decreases (Da) and increases with slip parameter (α).

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